

# PDLAMMPS - made easy

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## 1 Peridynamic theory of solids

The peridynamic theory of solid mechanics (S. Silling, 2000; S. Silling, Zimmermann, & Abeyarante, 2003; S. A. Silling, Epton, Weckner, Xu, & Askari, 2007) has been proposed as an alternative to the classical theory, and is offered as a mathematically consistent technique for modeling solid bodies with continuous and discontinuous displacements as well as a method that unifies the mechanics of particles and continuum bodies through the utilization of long-range forces.

The balance equation between rate of change of linear momentum and applied force on a deformable body  $\Omega$  develops the fundamental equation in classical continuum mechanics is written in Eq. (1)

$$\rho(x)\ddot{u}(x,t) = \nabla \cdot \sigma + \mathbf{b}(x,t). \quad (1)$$

where,  $x \in \Omega$ ,  $t$  is the time,  $\rho$  is the mass density,  $\ddot{u}$  is the acceleration,  $\sigma$  is the stress tensor and  $b$  is the body force. This differential equation is not well defined at the discontinuities. The PD formulation of a continuum introduces integral form of kinematic equation in order to mitigate this issue by calculating the force density on each material point as

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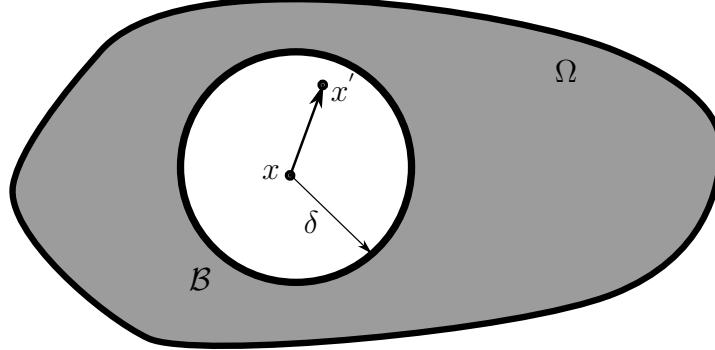


Figure 1: Schematic of peridynamic body.

$$\rho(x)\ddot{\mathbf{u}}(x,t) = \int_{\mathcal{B}} \mathbf{f}(\eta, \xi) dV + \mathbf{b}(x,t). \quad (2)$$

where, deformable body  $\Omega$  is represented with respect to an arbitrary frame of reference,  $\mathbf{f}$  is the pairwise force applied on particle at  $x$  by a neighborhood particle at  $x'$  and  $\mathcal{B}$  is a spherical region in the neighborhood of  $x$  with radius  $\delta$ ,  $\xi=x'-x$  and  $\eta=\mathbf{u}(x',t)-\mathbf{u}(x,t)$  are relative position and displacement vectors, respectively (Fig 1). For a certain  $\delta > 0$ ,  $\mathbf{f}(\eta, \xi) = 0$  for all  $\eta$  when  $\|\xi\| > \delta$ . This equation may be written more elaborately in terms of bond between  $x$  and  $x'$  as

$$\rho(x)\ddot{\mathbf{u}}(x,t) = \int_{\mathcal{B}} \left\{ \underline{\mathbf{T}}[x,t] \langle x' - x \rangle - \underline{\mathbf{T}}[x',t] \langle x - x' \rangle \right\} dV_{x'} + \mathbf{b}(x,t). \quad (3)$$

Equation. 3 is Newton,s equation of motion for continuum node  $x$ . The left hand side of Eq. 3 is *MassDensity*  $\times$  *Acceleration* and the right hand side of Eq. 3 corresponds to force density. Equation. 3 can be written in discretized form as (Parks, Lehoucq, Plimpton, & Silling, 2008)

$$\rho_i \ddot{\mathbf{u}}_i = \sum_{j \neq i}^{\mathcal{M}_\delta} \{ \underline{\mathbf{T}}[x_i,t] \langle x_j - x_i \rangle - \underline{\mathbf{T}}[x_j,t] \langle x_i - x_j \rangle \} \Delta V_{x_i} + \mathbf{b}_i. \quad (4)$$

Here,  $\|x_j - x_i\| \leq \delta$ .  $\mathcal{M}_\delta$  correspond to number of peridynamic nodes within the horizon  $\delta$ . The force vector state  $\underline{\mathbf{T}}[x,t]$  is interpreted in terms

of mapping the bond between  $x_i$  and  $x_j$  to a force per volume which has a cutoff range. Each particle experiences two types of forces: short range forces and long range forces i.e. bond-forces. Short range forces are repulsive in nature. The bond-force on each particle is generated from the bonds it shares with the neighboring particles. Here, the  $\underline{\mathbf{T}}$  is an infinite dimensional vector operator that maps the deformed image of the vector contained in the angle brackets,  $\langle \rangle$ , into the force acting on  $x$ .  $\underline{\mathbf{T}} = \underline{t}\underline{\mathbf{M}}$  is defined as a *force vector-state*.  $\underline{t}$  and  $\underline{\mathbf{M}}$  are the scalar force state and deformed state, respectively. In PDLAMMPS the bond based peridynamics is implemented as prototype microelastic brittle model (**PMB**). The scalar force state for *PMB* is written as (Parks et al., 2008; S. Silling, 2000)

$$\underline{t}_{PMB} = \frac{1}{2} \frac{18K}{\pi \delta^4} \frac{\|\eta + \xi\| - \|\xi\|}{\|\xi\|}. \quad (5)$$

For the state-based peridynamic linearly elastic (**LPS**), elastic-plastic (**EPS**) and viscoelastic (**VES**) solids the scalar force state is written as (Parks et al., 2008; S. A. Silling et al., 2007)

$$\underline{t}_{Elastic} = -\frac{3K\theta}{m} \underline{\omega}x + \alpha \underline{\omega}e^d, \quad (6)$$

$$\underline{t}_{Plastic} = -\frac{3K\theta}{m} \underline{\omega}x + \alpha \underline{\omega}(e^d - \underline{e}^{dp}), \quad (7)$$

$$\underline{t}_{Viscoelastic} = -\frac{3K\theta}{m} \underline{\omega}x + (\alpha_\infty + \alpha_i) \underline{e}^d - \alpha_i \underline{\omega}e^{db(i)}. \quad (8)$$

In Eq. 6  $\underline{\omega}\langle\xi\rangle$ ,  $\underline{x}\langle\xi\rangle = \|\xi\|$  where  $\xi = \mathbf{x}' - \mathbf{x}$ .  $m$ ,  $\theta$ ,  $e$  and  $e^d$  are the influence function, reference state, weighted volume, dilatation, extension state and deviatoric extension state respectively. The bulk modulus is  $K$  and the shear modulus ( $G$ ) related term  $\alpha = \frac{15G}{m}$  (S. A. Silling et al., 2007). In the above equations  $\underline{e}^{dp}$  is the plastic component of the extension state,  $\underline{e}^{db(i)}$  is the back extension state. For viscoelasticity model  $\alpha = \alpha_\infty + \alpha_i$  and  $0 < \alpha_i < \frac{15\mu}{m}$  (Parks et al., 2008; Mitchell, 2011a, 2011b). The detail about the peridynamic models implemented in PDLAMMPS can be found in the PDLAMMPS-documentation (Parks et al., 2008) and EPS and VES documentations (Rahman & Foster, 2013a, 2013b).

## 2 Implementation of peridynamics in LAMMPS

As the discretized version of the governing equation in peridynamics (Eq. 4) is a Newton's equation of motion, peridynamics was implemented in the classical molecular dynamics package LAMMPS (Parks et al., 2008; Plimpton, 1995). The peridynamics implementation in LAMMPS is known as *PDLAMMPS*. The package *PERI* in the LAMMPS *src* directory contains four peridynamic pair-styles: pmb, lps, eps and ves. *PERI* can be compiled as follows

```
$ make yes-peri  
$ make foo
```

Here, *foo* corresponds to the machine name you are building LAMMPS for. For more information please look at the LAMMPS compilation instructions at [http://lammps.sandia.gov/docSection\\_start.html#start\\_2](http://lammps.sandia.gov/docSection_start.html#start_2).

### 2.1 Linear peridynamic soild: LPS

The formulation for *peri-lps* (Eq.6) was applied in PDLAMMPS. The pair style for *lps* is

```
pair_style peri/lps  
pair_coeff * * K G horizon s00 Constant_alpha
```

Here,  $K$ ,  $G$ ,  $\text{Constant-}s_{00}$  and  $\text{Constant-}\alpha$  are the bulk modulus, shear modulus and bond-breaking constants, respectively.<sup>1</sup> The unit for  $K$  and  $G$  is  $\frac{\text{Force}}{\text{Area}}$ .  $\text{Constant-}s_{00}$  and  $\text{Constant-}\alpha$  are **unit-less**. The horizon  $\delta$  is in the unit of *Length*.

### 2.2 Peridynamic elastic-plastic soild: EPS

The formulation for *peri-eps* (Eq.7) was applied in PDLAMMPS. The pair style for *eps* is (Rahman & Foster, 2013a)

```
pair_style peri/eps  
pair_coeff * * K G horizon s00 alpha YieldStress
```

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<sup>1</sup>The user must not get confused with the completely different parameters:  $\text{Constant-}\alpha$  and  $\alpha = \frac{15G}{m}$ .

Here,  $K$ ,  $G$ , Constant- $s_{00}$  and Constant- $\alpha$  are the bulk modulus, shear modulus and bond-breaking constants, respectively.  $YieldStress$  is the material's yield stress  $\sigma_Y$ . The unit for  $K$ ,  $G$  and  $\sigma_Y$  is  $\frac{Force}{Area}$ . Constant- $s_{00}$  and Constant- $\alpha$  are ***unit-less***. The horizon  $\delta$  is in the unit of *Length*.

### 2.3 Peridynamic visco-elastic soild: VES

The formulation for *peri-ves* (Eq.8) was applied in PDLAMMPS. The pair style for *ves* is (Rahman & Foster, 2013b)

```
pair_style peri/ves
pair_coeff * * K G horizon s00 alpha lambda_i tau_i
```

Here,  $K$ ,  $G$ , Constant- $s_{00}$  and Constant- $\alpha$  are the bulk modulus, shear modulus and bond-breaking constants, respectively. Constant- $\lambda_i$  and Constant- $\tau_i$  are the viscoelastic relaxation parameter and time constant, respectively. The unit for  $K$  and  $G$  is  $\frac{Force}{Area}$ . Constant- $s_{00}$ , Constant- $\alpha$ , Constant- $\lambda_i$  and Constant- $\tau_i$  are ***unit-less***. The horizon  $\delta$  is in the unit of *Length*.

### 2.4 Peridynamic prototype microelastic brittle solid: PMB

The formulation for *peri-pmb* (Eq.5) was applied in PDLAMMPS. The pair style for *pmb* is

```
pair_style peri/pmb
pair_coeff * * c horizon s00 alpha
```

Here,  $c = \frac{18K}{\pi\delta^4}$ , Constant- $s_{00}$  and Constant- $\alpha$  are the spring constant and bond-breaking constants, respectively. The unit for  $c$  is  $\frac{Energy}{Length^7}$ . Constant- $s_{00}$  and Constant- $\alpha$  are ***unit-less***. The horizon  $\delta$  is in the unit of *Length*.

## 3 Consistent units in PDLAMMPS

In PDLAMMPS the units must be consistent with the available LAMMPS units. Let,  $K$ ,  $G$ ,  $\delta$  are the bulk-modulus, shear modulus and horizon, respectively.  $\tilde{\mathbf{f}}$  and  $\mathbf{r}_{IJ}$  are the force density vector at a node and distance between  $I^{th}$  and  $J^{th}$  peridynamic nodes, respectively. These later two parameters can be obtained after running PDLAMMPS (e.g. *LAMMPS dump file*).

For an example, in ***si*** and ***metal*** units the set of consists units are shown in Table. 1. For other LAMMPS units the user must follow the required unit consistency in LAMMPS.<sup>2</sup>

	Metal	Si
$K$	$\text{eV}/\text{\AA}^3$	Pascals
$G$	$\text{eV}/\text{\AA}^3$	Pascals
$\delta$	$\text{\AA}$	Meters
$\tilde{\mathbf{f}}$	$\text{eV}/\text{\AA}^4$	Newton/Cubic meters
$\mathbf{r}_{IJ}$	$\text{\AA}$	Meters

Table 1: Difference between consistent units in PDLAMMPS

## 4 Additional features in PDLAMMPS

In PDLAMMPS there are three *compute* commands available. The command ***compute damage/atom*** calculates the damage  $\phi(\mathbf{x}, t)$  at each peridynamic node (Parks et al., 2008). The peridynamic damage can be expressed as

$$\phi(\mathbf{x}, t) = 1 - \frac{\int_{\mathcal{H}} \mu(t, \eta, \xi) dV_{x'}}{\int_{\mathcal{H}} dV_{x'}} \quad (9)$$

$$s_0(t, \eta, \xi) = s_{00} - \alpha s_{min}(t, \eta, \xi) \quad (10)$$

$$s_{min}(t) = \min_{\xi} s(t, \eta, \xi) \quad (11)$$

Here,  $\mu(t, \eta, \xi)$  is a binary function.

$\mu(t, \eta, \xi) = 1$  if  $s'(t', \eta, \xi) < \min(s_0(t', \eta, \xi), s_0(t', \eta', \xi))$  for  $0 \leq t' \leq t$ . Otherwise,  $\mu(t, \eta, \xi) = 0$ . And,  $\xi' = x'' - x'$  and  $\eta' = \mathbf{u}(x'', t) - \mathbf{u}(x', t)$ . The Eq. 9 refers to the accumulation of damages at a node while each bond stretch exceeds the critical bond stretch  $s_0(t, \eta, \xi)$ . The material dependent parameters Constant- $s_{00}$  and Constant- $\alpha$  are used in Eq. 11. During the simulation the values for  $\phi(\mathbf{x}, t)$  varies within the interval  $[0, 1]$

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<sup>2</sup>For detail information the user is referred to <http://lammps.sandia.gov/doc/units.html>.

Another compute command is ***compute dilatation/atom***. The dilatation  $\theta(\mathbf{x}, t)$  is written as (S. A. Silling et al., 2007)

$$\theta(\mathbf{x}, t) = \frac{3}{m(\mathbf{x}, t)} \int_{\mathcal{B}} \underline{\omega}(\xi) \underline{x}(\xi) \underline{e}(\xi) dV_{\xi} \quad (12)$$

$$m(\mathbf{x}, t) = \int_{\mathcal{B}} \underline{\omega}(\xi) \underline{x}(\xi) \underline{x}(\xi) dV_{\xi} \quad (13)$$

It is observed from Eq. 12 and 13 that  $\theta(\mathbf{x}, t)$  is ***unit-less*** and it varies within the interval  $[0, \infty)$ . This compute command is applicable to *peri-lps*, *peri-eps* and *peri-ves*.

The third compute is ***compute plasticity/atom***. This compute is applicable to only *peri-eps*. At each time-step ***compute plasticity/atom*** calculates and stores the plasticity parameter  $\lambda$  for each peridynamic node.  $\lambda$  refers to the plasticity consistency parameter. From Eq. 7 the deviatoric component of the scalar force state is  $\underline{t}_{Plastic}^d = \alpha \underline{\omega}(\underline{e}^d - \underline{e}^{dp})$ . In order to obtain the constitutive model based on plasticity the allowable deviatoric force state  $\underline{t}_{Plastic}^d$  satisfies the inequality  $\psi(\underline{t}_{Plastic}^d) - \psi_0 \leq 0$ . Preferably,  $\psi(\underline{t}_{Plastic}^d) = \frac{\|\underline{t}_{Plastic}^d\|^2}{2}$ . Here,  $\psi_0 \leq 0$  is the yield point of the material. Based on the plastic flow rule  $\dot{e}^{dp} = \lambda \nabla^d \psi$ .  $\nabla^d \psi$  is the constrained Frèchet derivative of  $\psi$  while the previously mentioned inequality is satisfied. For detail derivations please look at the document provided by John Mitchell at Sandia national lab (Mitchell, 2011a).  $\lambda$  is ***unit-less*** and varies within the interval  $[0, \infty)$ . All three of these computes store the values in C++ one dimensional arrays or vectors.

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